Qualifying Frac Sand Resources Using Cutting Edge Technology







Sample prep & handling Data correlation PSD as decision tool PSD for "fingerprinting"







& Conclusions



- ষ Quick
- ন্থ Reliable
- ষ 21st Century upgrade for PSD and more
- *σ* Sample Handling Key to Reproducible Results
- ø Natural variability on material is different that
 manufactured product
- ø Use statistics & trend charts for big data sets vs.
 time







Prospecting











•	PHI - m COVERS log ₂ (d)	m ION In mmij Imm	Inche II	SIZE	after	SI	EVE	notes ins a size	Nur of g	mber rains	Sett Velo	ling	Thre	shold
h		100	the state	Went	worth,1922	P		1998	per	mg	20	C)	Cm	/sec
4			EB	-	+	원험	2 S	229	- 11 E E	1	-Ê	1.526	1040	ES
7-	-200	128	- 10.1"	90	(ASTM (U.S. Sta	Mosh	Intermedia of nation	Quartz	Naturel	Spheres Dibo, 19	Defait	(hurdin, 19-46	incided for
6-	Ē.	64.0 53.9	-2.52"			-2 1/2*	- 94					I	- 200	1 m above bottor
5-	-10	45.3 33.1 32.0	-1.26*		coarse	-1 1/2"	E1 1/2*						- 150	
	-20	26.9 22.6 17.0			coarse	- 1.06"	- 1.05*				100	50		
4-	_10	16.0 13.4 11.3 9.52	-0.63*	BLEE	medium	- 5/8" - 1/2" - 7/16" - 3/8"	.525"				- 90	- 40	- 90	
3-	E -	8.00 6.73 5.66	- 0.32*	E	fine	- 265-	E a				- 60		- 70	
2-	4 -	4.76 4.00 3.36 2.83	-0.16*	15	vory	4567	45 67				- 50 - 40	- 20	- 60	- 100
1-	-2 -	2.38	-0.08*		Granulos	- 8	- 8				- 30		- 50	
	F. 3	1.63 1.41 1.19	mm		coarse	12	- 10 - 12 - 14	. 1 2			- 20	- 10	- 40	- 50
	E' E	.840 .707 .545	L.		COBPSE	20	20 24 28	86	- 2.0	- 1.5	- 10	87	- 30	- 40
1-	5 -	.500 .420 .354	- 1/2	AND	medium	- 35 - 40 - 45	- 32 - 35 - 42	59 42	- 5.6	- 4.5	8766	- 5		- 30
2-	2	.297 .250 .210	- 1/4	S	tine	- 60 - 70 - 20	- 60 - 65 - 80	30	- 43	- 35	- 3	- 3	- 20	- 26
3 -	1, -	.149	- 1/8		-	- 100 - 120 - 140	- 100 - 115 - 150	155	- 350	- 240	= 1	- 1.0	(inmar	mum 1,1949)
4-	E :	.088	- 1/16		fine	- 170	- 170 - 200 - 250	115	-1000	- 580	0.5	0.5	75-01W	
5-	05	.053	- 1/32		coarse	- 325	- 325	-			0.1		ocity ocity	uo p
	02	2 2.299		5	medium	differ	by as scale	2		٩		(Må	he be	a pa
6-	01	_016	- 1/64	15	tine	nings m sca	atte	gular		gular	- 0.023	R = 6x1	noon	tions.
7-	E oos	.009	-1/128		very	phi m	nings hig mo	o suba quartz m)		s uba	-0.0067	Law (not not	thy is i
8-	004 -	.004	-1/256		Clay/Sitt boundary	r from	4 %	in miles to		Inded to	-0.0014 -0.001	Sto kee	matter to the	on the
9-	002	.002	- 1/512	CLAY	analysis	slightly	uch as	ste: App		abroa	-0.00036		of tract	that the



PERFORMING A SIEVE ANALYSIS

- You can begin your particle size distribution analysis after you properly collect, prepare and size a sample.
- Select test sieves with mesh openings that reveal particle distribution at critical sizes. These are usually stated.
- in a product specification or determined by material processing requirements.

To perform the analysis, do the following:

- I. Stack the sieves on top of each other with the coarsest (largest) opening on the top of the stack.
- 2. Put a bottom pan under the finest (smallest) opening sieve. This pan collects "fine" material that passes through the last one.
- 3. Use a laboratory scale (accurate to .1 gram) to weigh an empty container (such as an extra empty bottom pan) and establish the tare weight.
- 4. Weigh the sample material.
- 5. Empty the sample into the top of the stack. Make sure you do not overload the surface as this causes "blinding" or blocking of the openings.
- Put the stack into the sieve shaker.

- 7. Place a cover on the top of the stack.
- 8. Make sure the stack is securely in place.
- 9. Set the proper length of time to agitate the material.
- 10. Turn on the shaker and run the test.
- 11. After the shaker stops, empty the material from the coarsest sieve into the empty container that you weighed in step (3). Use a soft bristle brush to gently brush the underside of the sieve to remove all of the particles.
- 12. Tap the side of the frame with the handle of the brush to clean the remaining material from the sieve.
- Weigh the contents in the pan to the nearest 1/10 gram and record the data.
- 14. Return the material to its original sample container.
- 15. Repeat steps 11 through 14, using the container referenced in step (3) for each sieve, including the fine material in the bottom pan.
- 16. Total the weights to make sure the sum of the retained material and the material in the bottom pan is as close as possible to the original weight. Check your specification for allowable variation.
- 17. Divide the weight obtained from each sieve by the weight of the original sample. Record the percentage for each sieve.
- 18. Calculate and record the cumulative percentages as required.



ISO 13503-2/API 19/56











*Gert Beckmann Retsch Technology 15



"representative sample...."









Camsizer vs. Rotap learnings

 NEVER scoop always use sample splitter
 No mechanical agitation like RoTap
 Clusters and "coating" source for discrepancy

& Smaller sample size – unforgiving!!



Sample prep

Air dry Split & weigh Wash, wet sieve – P200 Dry and calculate %loss Micro photograph Archive sample









Mean Partial Size





×113

22

10.00

Plot Area

1.00

Gradation Analysis





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Proving the "method..."

- Creating a "standard" sample
- Splitting "standard" sample maintain representative
- Confirm to "ISO equivalence"
- Establish statistically significant like vs. different



Split sample into 5 parts. 4 splits used for ro-tap. 1 split used exclusively for CAMSIZER

Run 3 of 4 samples in the ro-tap individually - once (saved 2, 3 and 4 to run through the CAMSIZER)

Run 4th sample three times through ro-tap Split the one sample used for the CAMSIZER into 4 smaller parts

Run 3 of 4 samples through the CAMSIZER once

Run the 4th sample through the CAMSIZER three times

Run sample 2, 3, and 4 from the ro-tap through the CAMSIZER



1			Raw Sand (wor	newoc)							
			Standard Samp	le							
1											
			V								
Sample A	Sample B	Sample C	Sample D	Sample D	Sample D	Sample D	Sample E				
							V				
1											
1					Sample E1	Sample E2	Sample E3	Sample E4	Sample E4	Sample E4	



Same split sample using sieves

Ro-tap							
	а	b	с	d	d	d	
Sieve Size	Sample 1	Sample 2	Sample 3	Sample 4	Sample 4	Sample 4	
(US Stand	(%)	(%)	(%)	(%)	(%)	(%)	
16	0.3	0.3	0.2	0.2	0.5	0.1	
18	0.5	0.8	0.6	0.7	0.8	0.6	
20	2.2	2.4	2.3	2.4	2.3	2.3	
25	6.8	7.6	6.9	7.3	7.4	7.4	
30	13.6	13.9	13.9	13.9	13.8	13.6	
35	18.6	18.8	18.9	19.0	18.8	19.4	
40	21.2	20.9	21.1	20.8	20.9	20.5	
45	20.7	20.3	20.7	20.7	20.3	20.6	
50	12.0	11.6	11.6	11.8	11.9	12.0	
60	2.9	2.7	2.8	2.7	2.6	2.7	
70	0.4	0.5	0.5	0.3	0.3	0.4	
100	0.4	0.5	0.4	0.4	0.3	0.5	
200	0.0	0.1	0.0	0.0	0.0	0.0	
Pan	0.0	0.1	0.0	0.0	0.2	0.1	
	99.6	100.5	99.9	100.0	99.9	100.0	



CAMSIZER

Test 1	Test 2	Test 3	Test 4	Test 4	Test 4	Test 7 - Sa	Test 8 - Sa	a Test 9 - Sa	mple 4
(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	
0.3	0.8	0.2	0.3	0.4	0.3	0.4	0.2	0.3	
1.2	0.9	0.9	0.7	1.1	0.8	0.9	1.1	1.1	
2.7	2.8	2.5	2.8	2.8	2.8	2.8	3.0	2.9	
8.5	8.8	8.0	7.7	7.6	8.0	8.3	8.1	8.7	
13.3	13.3	12.8	12.9	12.9	12.8	12.2	13.7	13.2	
20.8	20.9	20.4	21.1	20.4	19.9	21.0	21.2	19.1	
21.4	21.1	22.0	20.9	21.3	21.1	22.1	20.2	21.2	
19.4	19.5	20.1	20.0	19.9	20.9	19.7	19.2	20.8	
8.8	8.4	9.0	9.4	9.6	9.1	8.8	9.3	9.0	
2.7	2.5	3.0	3.1	2.8	3.1	2.8	2.9	2.7	
0.5	0.6	0.7	0.7	0.7	0.7	0.6	0.7	0.6	
0.3	0.3	0.3	0.3	0.4	0.4	0.3	0.3	0.3	
0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	



Same sample 3x Rotap



Same sample 3x Camsizer



All sets of Rotap data



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All Sets of Camsizer data





Average of all Camsizer - Blue Rotap - Red

ID	Method	20/40 w	ı/ 95% Cl	Variance
ABC	Sieve	58.9	62.5	3.5
E4(3x)	Camsizer	60.1	64.3	4.3
D(3x)	Sieve Only	59.4	62.3	2.9
E4(3x)	Camsizer	60.1	64.3	4.3
All Samples	Both	56.9	67.3	10.4
E1E2E3E4(3x)+BCD	Camsizer	58.8	67.2	8.4
ABCD(3x)	Sieve	58.8	62.7	3.9
D(3x)	Sieve	59.4	62.3	2.9
D(1x) recombined	Camsizer		62.2	
D(3x Sieve)+1x Cam	Both	57.8	64.7	6.9







March 26,2013



Round/Sphericity....Proving the "method..."













Roundness/Sphericity





Sphericity							average(dup1-5)	average(dup1-5+org	S.D.(dup1-5)	S.D.(dup1-5+org)	CI(F-2)	
	org	dup1	dup2	dup3	dup4	dup5						
16	0.858	0.958	0.939		0.838	0.906	0.91025	0.8998	0.052740718	0.051304971	0.1054	8 0.10261
18	0.88											
20	0.845	0.839	0.864	0.815	0.838	0.845	0.8402	0.841	0.01754138	0.015811388	0.0350	8 0.03162
25	0.831	0.771	0.795	0.772	0.803	0.779	0.784	0.791833333	0.014317821	0.023068738	0.0286	4 0.04614
30	0.778	0.771	0.801	0.763	0.781	0.78	0.7792	0.779	0.014219705	0.012727922	0.0284	4 0.02546
35	0.763	0.742	0.762	0.766	0.762	0.76	0.7584	0.759166667	0.009423375	0.008635199	0.0188	5 0.01727
40	0.764	0.741	0.755	0.736	0.738	0.756	0.7452	0.748333333	0.009576012	0.011500725	0.0191	5 0.023
45	0.749	0.741	0.746	0.736	0.741	0.733	0.7394	0.741	0.005029911	0.005966574	0.0100	6 0.01193
50	0.732	0.718	0.728	0.719	0.724	0.724	0.7226	0.724166667	0.00409878	0.005307228	0.008	2 0.01061
60	0.721	0.717	0.714	0.713	0.712	0.709	0.713	0.714333333	0.002915476	0.004179314	0.0058	3 0.00836
70	0.71	0.696	0.699	0.7	0.702	0.698	0.699	0.700833333	0.002236068	0.00491596	0.0044	0.00983

s						average(c	average(d	S.D.(dup1	S.D.(dup1-	5+org)	CI(F-2)	
org	dup1	dup2	dup3	dup4	dup5							
0.665	1	1		0.975	0.625	0.9	0.853	0.18371	0.19068			
0.84												
0.845	0.653	0.913	0.747	0.791	0.69	0.7588	0.77317	0.1011	0.09703		0.20219	0.19406
0.822	0.71	0.809	0.782	0.724	0.744	0.7538	0.76517	0.04106	0.04609		0.08213	0.09218
0.801	0.745	0.747	0.74	0.773	0.714	0.7438	0.75333	0.02102	0.02998		0.04203	0.05996
0.782	0.774	0.753	0.759	0.769	0.727	0.7564	0.76067	0.01838	0.01948		0.03676	0.03896
0.762	0.726	0.756	0.722	0.722	0.733	0.7318	0.73683	0.01425	0.01774		0.02851	0.03547
0.716	0.703	0.725	0.704	0.7	0.675	0.7014	0.70383	0.01778	0.01699		0.03557	0.03397
0.684	0.67	0.679	0.679	0.68	0.664	0.6744	0.676	0.00709	0.00746		0.01418	0.01491
0.653	0.648	0.654	0.653	0.653	0.639	0.6494	0.65	0.00627	0.0058		0.01254	0.01159
0.621	0.613	0.627	0.624	0.623	0.597	0.6168	0.6175	0.01226	0.0111		0.02451	0.02219
	s org 0.665 0.84 0.845 0.822 0.801 0.782 0.762 0.716 0.684 0.653 0.621	s dup1 org dup1 0.665 1 0.845 0.653 0.845 0.653 0.822 0.714 0.801 0.745 0.782 0.726 0.762 0.726 0.716 0.703 0.684 0.67 0.653 0.648	s dup1 dup2 org dup1 dup2 0.665 1 1 0.845 0.653 0.913 0.845 0.653 0.913 0.822 0.71 0.809 0.822 0.74 0.753 0.801 0.745 0.747 0.752 0.726 0.756 0.762 0.703 0.725 0.684 0.67 0.679 0.653 0.648 0.654	sImage: line systemorgdup1dup2dup30.6651110.8450.6530.9130.7470.8450.6530.9130.7470.8220.710.8090.7820.8010.7450.7470.7820.7820.7740.7530.7590.7620.7030.7250.7040.6840.670.6790.6790.6530.6480.6530.6530.6210.6130.6270.624	simageimageimageimageorgdup1dup2dup3dup40.6651110.9750.840.6530.9130.7470.7910.8450.6530.9130.7470.7240.8220.710.8090.7820.7240.8010.7450.7470.7410.7730.7620.7740.7530.7590.7690.7620.7030.7550.7040.7220.6840.6670.6590.6530.6530.6530.6480.6540.6530.6530.6210.6130.6270.6240.623	sImage: line systemorgdup1dup2dup3dup4dup50.665110.9750.6250.840.6530.9130.7470.7910.690.8450.6530.9130.7470.7910.690.8220.710.8090.7820.7240.7440.8010.7450.7470.740.7410.7410.8020.7140.7530.7250.7220.7270.7620.7260.7560.7220.7330.6530.6840.670.6790.6690.6530.6540.6530.6480.6540.6530.6530.6390.6210.6130.6270.6240.6230.597	s Image: solution of the solution of t	simage: def constraint of the sector of the sec	simage: second seco	simage: solution indeximage: solution indexsolution indexorgdup1dup2dup3dup4dup5image: solution index0.6651111image: solution index0.6250.090.8330.183710.190680.8440.6530.9130.7470.7910.625image: solution index0.75380.773170.10110.097030.8450.6530.9130.7470.7910.649image: solution index0.75380.75170.01010.097030.8420.7110.8490.7820.7240.744image: solution index0.75380.75170.01010.097030.8420.7140.8490.7530.7470.7490.744image: solution index0.75380.75330.01020.02980.7820.7740.7490.7530.7470.7490.743image: solution index0.14580.14580.01420.014980.7830.7740.7590.7690.7690.7670.764image: solution index0.1458image: solution index0.14580.7840.7740.7750.7740.7730.7740.774image: solution indeximage: solution indeximage: solution index0.7840.7740.7750.7740.7750.7740.774image: solution indeximage: solution indeximage: solution index0.7840.7740.7750.7740.7750.7740.774image: solution index<	simageimag	simageimag







	Site 1			Site 2			Site 3		5	Site 4			
Sieve Size (US Standard)	% Retained	Roundness	Sphericity										
#16	0.1	0.92	0.96	0.4	0.91	0.87	0.3	0.91	0.87	0.6	0.67	0.86	
#18	0.1	0.83	0.88	0.4	0.87	0.90	0.7	0.87	0.90	1.1	0.84	0.88	
#20	0.8	0.75	0.85	1.1	0.83	0.87	1.5	0.83	0.87	1.7	0.85	0.85	
#25	2.2	0.77	0.81	3.5	0.77	0.83	4.1	0.77	0.83	4.1	0.82	0.83	
#30	6.6	0.78	0.83	5.2	0.82	0.83	7.2	0.82	0.83	6.3	0.80	0.78	
#35	14.6	0.76	0.78	9.1	0.79	0.78	11.5	0.79	0.78	8.8	0.78	0.76	
#40	17.6	0.73	0.77	10.2	0.79	0.77	12.7	0.79	0.77	9.7	0.76	0.76	
#45	22.9	0.74	0.75	12.9	0.76	0.76	14.2	0.76	0.76	11.6	0.72	0.75	
#50	20.0	0.70	0.72	10.2	0.72	0.73	11.4	0.72	0.73	10.2	0.68	0.73	
#60	10.3	0.65	0.71	8.2	0.67	0.72	9.6	0.67	0.72	10.2	0.65	0.72	
#70	2.2	0.61	0.70	5.3	0.63	0.70	5.7	0.63	0.70	7.2	0.62	0.71	
#100	0.8	0.34	0.63	7.9	0.23	0.49	6.4	0.23	0.49	9.3	0.49	0.61	
#200	0.4	0.19	0.54	16.5	0.22	0.43	8.1	0.22	0.43	11.3	0.24	0.38	
PAN	1.5			9.2			6.6			8.0			
20/40	41.0	0.7595	0.797	28.0	0.79275	0.79925	35.6	0.79275	0.79925	28.9	0.79175	0.784	
30/50	75.1	0.7	0.8	42.4	0.8	0.8	49.8	0.8	0.8	40.3	0.7	0.8	
40/70	55.3	0.7	0.7	36.6	5 0.7	0.7	40.9	0.7	0.7	39.2	0.7	0.7	





TECHNICAL COMMUNICATION

GRADISTAT: A GRAIN SIZE DISTRIBUTION AND STATISTICS PACKAGE FOR THE ANALYSIS OF UNCONSOLIDATED SEDIMENTS

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GradStat8

	SAMDLE STATISTICS				
	SAMPLE STATISTICS				
		1	2	3	4
	ANALYST AND DATE:				
	SIEVING ERROR:				
	SAMPLE TYPE:	Unimodal, Well Sorted	Bimodal, Moderately Sorted	nimodal, Moderately Sorte	nimodal, Moderately Sorte
	TEXTURAL GROUP:	Sand	Sand	Sand	Sand
	SEDIMENT NAME:	Well Sorted Medium Sand	derately Sorted Medium Sa	derately Sorted Medium Sa	lerately Sorted Medium S
METHOD OF	MEAN (😎 🚬 💙 :	428.4	363.2	407.0	386.5
MOMENTS	SORTING (C ~ ~)	I 137.7	210.9	203.0	228.2
Arithmetic (µm)	SKEWNESS (SKC.)	: 1.473	1.341	1.161	1.529
	KURTOSIS (K _)	9.001	7.112	6.321	7.217
METHOD OF	MEAN < 🖂 🚬 🔪 :	406.9	301.0	353.9	323.4
MOMENTS	SORTING (-)	= 1.361	1.873	1.726	1.829
Geometric (µm)	SKEWNESS (STAL)	= -0.068	-0.342	-0.581	-0.258
	KURTOSIS (K _)	= 4.255	2.249	3.068	2.549
METHOD OF	MEAN 🤇 😎 🪙 💙	= 1.297	1.732	1.499	1.629
MOMENTS	SORTING COT 2	= 0.444	0.905	0.787	0.871
Logarithmic (ø)	SKEWNESS (STA-	= 0.068	0.342	0.581	0.258
	KURTOSIS (IC	= 4.255	2.249	3.068	2.549
FOLK AND	MEAN (AZ -)	z 408.7	296.1	363.9	324.9
WARD METHOD		= 1.346	1.944	1.724	1.870
(μm)	SKEWNESS (Stag)	- 0.086	-0.276	-0.201	-0.156
	KURTOSIS (K.)	0.957	0.975	1.190	1.078
FOLK AND	MEAN (AZ -)	: 1.291	1.756	1.458	1.622
WARD METHOD	SORTING (C ,)	= 0.429	0.959	0.786	0.903
(ф)	SKEWNESS (SKEWNESS)	z -0.086	0.276	0.201	0.156
	KURTOSIS (K)	0.957	0.975	1.190	1.078
FOLK AND	MEAN:	Medium Sand	Medium Sand	Medium Sand	Medium Sand
WARD METHOD	SORTING:	Well Sorted	Moderately Sorted	Moderately Sorted	Moderately Sorted
(Description)	SKEWNESS:	Symmetrical	Fine Skewed	Fine Skewed	Fine Skewed
	KURTOSIS:	Mesokurtic	Mesokurtic	Leptokurtic	Mesokurtic

GradStat8

SAMPLE STATISTICS					
	1	2	3	4	
ANALYST AND DATE:	1	1	,	,	
SIEVING ERROR:					
SAMPLE TYPE:	Unimodal, Well Sorted	Bimodal, Moderately Sorted	nimodal, Moderately Sorte	nimodal, Moderately Sort	ed
TEXTURAL GROUP:	Sand	Sand	Sand	Sand	
SEDIMENT NAME:	Well Sorted Medium Sand	derately Sorted Medium Sa	derately Sorted Medium S	erately Sorted Medium S	and
MODE 1	≃ 390.0	390.0	390.0	390.0	
MODE 2 (µm):		112.5			
MODE 3 (µm):					
MODE 1 (¢):	1.364	1.364	1.364	1.364	
MODE 2 (\$):		3.237			
MODE 3 (ø):					
D ₁₀ (μm):	280.5	109.9	160.5	131.8	
D ₅₀ (μm):	401.4	339.5	380.6	342.5	
D ₉₀ (μm):	599.5	628.2	665.9	676.9	
(D ₉₀ / D ₁₀) (μm):	2.137	5.716	4.149	5.134	
(D ₉₀ - D ₁₀) (μm):	319.0	518.3	505.4	545.0	
(D ₇₅ / D ₂₅) (μm):	1.516	2.416	1.944	2.213	
(D ₇₅ - D ₂₅) (μm):	169.8	278.9	250.4	271.9	
D ₁₀ (φ):	0.738	0.671	0.587	0.563	
D ₅₀ (\$):	1.317	1.559	1.394	1.546	
D ₉₀ (φ):	1.834	3.186	2.639	2.923	
(D ₉₀ / D ₁₀) (φ):	2.484	4.750	4.500	5.192	
(D ₉₀ - D ₁₀) (φ):	1.096	2.515	2.053	2.360	
(D ₇₅ / D ₂₅) (φ):	1.598	2.188	2.004	2.133	
(D ₇₅ - D ₂₅) (ϕ):	0.600	1.272	0.959	1.146	

GradStat8 –cont.

Planning









Bore	%ret 20	%ret 30	%ret 40	%ret 50	% ret 60	%ret 70	%ret 100	% 20-40	% 30-50	% 40-70	%70-200	% >200	
TB-1 30-35	3.8	19.7	49.8	70.5	79.8	86.3	94.4	46.0	50.8	36.5	11.9	1.8	
TB-1 40-45	4.9	16.8	39.8	64.5	74.3	79.4	89.9	34.9	47.7	39.6	17.1	3.5	
TB-1 50-55	10.6	31.8	56.3	76.2	84.0	88.1	93.8	45.6	44.4	31.8	10.5	1.4	
TB-1 60-65	9.1	32.5	55.6	71.9	78.0	81.6	88.1	46.6	39.4	25.9	15.3	3.1	
TB-1 70-75	3.2	12.3	31.7	55.6	69.4	78.2	92.3	28.5	43.3	46.5	20.3	1.5	
TB-1 80-85	3.1	12.5	30.8	51.7	63.2	70.7	84.8	27.7	39.2	39.8	26.3	3.0	
TB-2 10-15	4.1	24.8	55.3	78.9	86.7	90.8	95.6	51.2	54.1	35.5	7.5	1.7	
TB-2 20-25	10.8	35.7	67.2	88.0	93.0	95.1	97.4	56.4	52.3	27.9	3.9	1.0	
TB-2 30-35	13.8	49.9	72.4	84.7	88.6	90.6	93.8	58.6	34.8	18.2	7.2	2.2	
TB-2 40-45	1.7	8.4	22.9	42.5	55.4	64.9	83.9	21.2	34.1	41.9	33.0	2.1	
TB-2 50-55	2.0	12.5	32.3	53.1	64.6	72.0	85.7	30.3	40.6	39.7	25.7	2.3	
TB-2 60-65	1.6	10.2	31.2	54.8	66.5	73.6	85.5	29.6	44.5	42.3	23.6	2.8	
TB-2 70-75	0.6	6.7	28.0	54.5	67.4	75.2	88.6	27.4	47.8	47.2	22.5	2.3	
TB-2 80-85	0.6	4.3	15.8	34.0	48.0	59.0	82.8	15.2	29.7	43.1	37.6	3.4	
TB-2 90-95	0.3	3.2	18.5	47.2	65.2	75.8	92.5	18.2	44.0	57.3	22.6	1.6	
TB-6 20-25	5.7	24.0	54.9	75.1	83.0	88.3	95.5	49.1	51.2	33.4	10.5	1.2	
TB-6 30-35	3.1	20.0	51.8	77.4	84.6	88.1	93.2	48.7	57.3	36.3	9.8	2.1	
TB-6 40-45	10.5	31.8	54.9	71.9	79.9	84.9	92.3	44.4	40.1	30.0	13.1	2.0	
TB-6 50-55	7.5	22.8	44.4	63.3	72.3	77.9	87.2	36.9	40.5	33.5	18.5	3.6	
TB-6 60-65	1.2	8.9	25.4	46.8	60.0	68.8	86.9	24.2	37.9	43.4	29.2	2.0	
TB-6 70-75	1.8	11.8	33.5	57.2	69.2	76.6	88.0	31.7	45.4	43.1	21.3	2.1	
TB-6 80-85	1.2	10.3	30.7	54.1	65.8	73.1	86.4	29.5	43.8	42.4	24.1	2.8	
TB-6 90-93	0.5	4.6	22.3	48.0	61.4	69.6	84.5	21.8	43.4	47.3	26.8	3.6	
TB-7 30-35	3.8	18.4	45.3	69.2	78.2	82.8	90.7	41.5	50.8	37.5	14.6	2.6	
TB-7 40-45	4.2	18.1	40.2	61.7	70.8	76.5	86.2	36.0	43.5	36.2	19.3	4.2	
TB-7 50-55	5.7	20.9	41.4	59.2	67.4	72.7	83.0	35.7	38.3	31.3	23.3	4.0	
TB-7 60-65	4.2	18.1	40.2	61.7	70.8	76.5	86.2	36.0	43.5	36.2	19.3	4.2	
TB-7 70-75	2.0	11.2	28.3	47.1	58.0	65.3	78.9	26.2	35.9	37.0	27.7	7.0	
TB-7 80-85	1.0	8.7	26.2	46.8	59.2	67.7	82.7	25.2	38.1	41.5	27.3	5.0	

					St. Peu	(MN 55180-5114		Sufface grade	eleivation:	~1052 ft amai			
Depth e In feet a	ELEV (ft amsi)	GRAPHIC LOG	MAJOR LITHOLOGY DESCRIPTIONS	Depth In feet	ELEV (FT AMSL)	GRAPHIC LOG	PE	ERCENT 20/70	0 100 0	PERCENT 20/40 100	"MEA DIAN 0	AN PARTICLE METER (MM) 1	PERCENT LOSS (< #200 MESH)
10 10 10 10 15 20 40 40 End of Bi	- 1046 -	s2 loss	Loess, brown Sendatore, soft, brown white, f, to cL, subergular to w fitnisted, moderating softed, trace eccessories, rare incl Sandatore, soft, buff, vfJ to cU, engular to well rounds poorly softed, name eccessories, name inclusions, name pr Sandatore, as above, predominantly ft, to miU Sandatore, soft, yellow coange, vfJ to miU engular to y nounded, fitnated, poorly softed, no eccessories, name pr Sandatore, soft, previow coange, vfJ to miU, engular to y nounded, fitnated, poorly softed, name accessories, name Sandatore, soft, previow, softed, name accessories, name Sandatore, soft, previow, vfJ to miU, angular to y nounded, fitnated, poorly softed, name accessories, name Sandatore, soft, buff orange, vfJ to cU, engular to well finated, bimodel, name accessories, name inclusions Sandatore, soft, wellow orange, vfJ to cU, engular to well finated, poorly softed, name accessories, name inclusions	0 5 10 15 20 30 35 40 45 55 60 70 75 80 76 80	1050 1045 1040 1035 1030 1025 1025 1025 1025 1020 1015 1010 1005 1000 995 990 995 990 995 990 995 997 975 970	1 62 feet.	77.3 78.3 73.7 70.6 65.7 58.0 64.3 63.3 60.8 69.5 76.0 73.3 73.4			28. 29. 29. 28. 33. 24. 29. 27. 30. 23. 38. 38. 38. 38. 30. 30. 30. 38.	1 2 7 5 8 1 2 9 9 2 2 9 9 9 9 9 9 9 9 9 9 9 9 9 9	0.38 0.38 0.38 0.36 0.41 0.35 0.35 0.35 0.35 0.37 0.33 0.39 0.39 0.39 0.39 0.41 0.46	4.2 4.8 7.8 8.5 7.9 10.3 9.0 9.2 9.2 10.4 8.8 5.4 8.1 7.6
Pag											pe 1 of 1		







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ArcGIS – Raster block allows x,y,z arithmetic





Block modeling

20-40 Interpolated Grade (1131-1140)







way 10, 2014



Data used to build.....

- 3d model of subsurface
- Estimate potential resource quantity
- Data gaps, uncertainty & risks
- Risk/benefit of additional data collection
- Resource Valuation Model (\$\$\$)

Ideal Proppant....

- Stronger than diamonds
- Lighter than water
- Cheaper than dirt
- Available everywhere



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